

2" (50 mm) exit compression driver for high sensitivity, low distortion and smooth extended frequency response applications. Its pure titanium diaphragm was especially designed based on the extremely light and structurally strong snowflake crystal. That leads the D408Ti driver to deliver high performance, high quality and high value for the pinnacle in sound reinforcement applications.

It combines a stable structure for mid-frequency reproduction and a low mass that enables high frequency reproduction virtually linear to 20 kHz.

Its construction features include:

- ferrofluid (Ferrosound®) loaded gap reducing heat build-up and offering consistent results over long-term demanding concert usage;
- voice coil is made of high temperature CCAW (copper clad aluminium wire) wound on Kapton® former to withstand high operating temperatures;
  - injected plastic housing;
- precisely engineered diaphragm structure and alignment mechanism allows for easy, reliable and cost effective repair (model RPD4400Ti) in case of diaphragm failure.



SPECIFICATIONS		
Nominal impedance		
Minimum impedance @ 3,450 Hz 6.3		
Power handling		
Musical Program(w/ xover 800 Hz 12 dB / oct) <sup>1</sup> 200	W	
Musical Program(w/ xover 1,200 Hz 12 dB / oct) <sup>1</sup> 250	W	
Sensitivity		
On horn, 2.83V@1m, on axis2	dB SPL	
On plane-wave tube, 0.0894V <sup>3</sup> 113	dB SPL	
Frequency response @ -10 dB 400 to 20,000	Hz	
Throat diameter	mm (in)	
Diaphragm material	Titanium	
Voice coil diameter	mm (in)	
Re4.8		
Flux density	T	
Minimum recommended crossover (12 dB / oct) 800	Hz	
<sup>1</sup> Power handling specifications refer to normal speech and/or music program material, reproduced by an amplifier producing no more than 5% distortion. Power is calculated as		

reproduced by an amplifier producing no more than 5% distortion. Power is calculated as true RMS voltage squared divided by the nominal impedance of the loudspeaker. This true RMS voltage squared divided by the nominal impedance of the loudspeaker. This voltage is measured at the input of the recommended passive crossover when placed between the power amplifier and loudspeaker. Musical Program= 2 x W RMS.

<sup>2</sup> Measured with HL4750-SLF horn, 800 -6,000 Hz average.

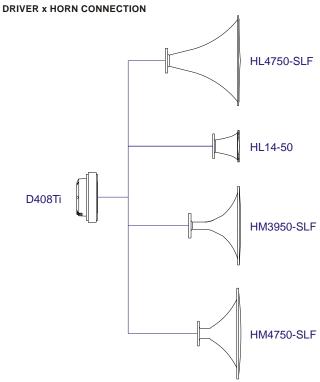
<sup>3</sup> The sensitivity represents the SPLin a 25 mm terminated tube, 400 - 3,000 Hz average.

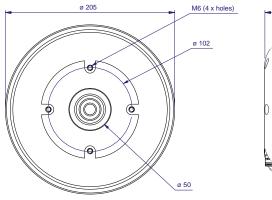
ADDIT	ONAL	INFORM	ATION

Magnet material		Barium ferrite
Magnet weight	2,640 (92)	g (oz)
Magnet diameter x depth 200 x 24	4 (7.87 x 0.95)	mm (in)
Magnetic assembly weight	7,860 (17.32)	g (lb)
Housing material		P lastic
Housing finish		Gray
Magnetic assembly steel finish		. Zinc-plated
Voice coil material		CCAW
Voice coil former material	Polyim	ide (Kapton®)
Voice coil winding length	6.0 (19.7)	m (ft)
Voice coil winding depth	2.0 (0.08)	mm (in)
Wire temperature coefficient of resistance ( ).	0.00404	1/°C
Volume displaced by driver		
voidino diopidoda by dirvoin	2.2 (0.078)	l (ft³)
Net weight		l (ft³) g (lb)
	8,540 (18.83)	` '

### MOUNTING INFORMATION

Horn connection	
Number of holes	4 (M6) equally spaced threaded holes
Threaded holes diameter	102 (4) mm (in)
Connectors	
Polarity	Positive voltage applied to the positive terminal
•	(red) gives diaphragm motion toward the throat

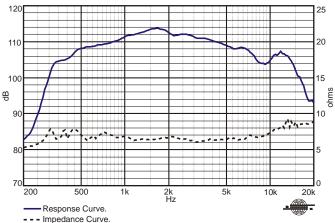




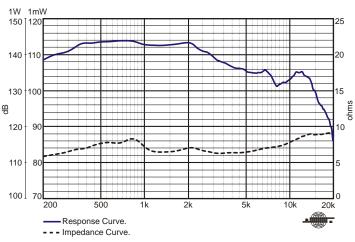
# PROFESSIONAL LINE - Compression Driver

## **D408Ti**

## RESPONSE AND IMPEDANCE CURVES W/ HL4750-SLF HORN INSIDE AN ANECHOIC CHAMBER, 1 W / 1 m $\,$

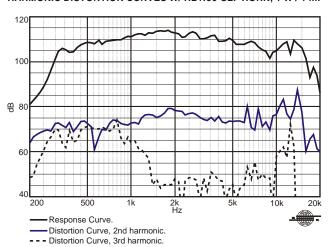


## RESPONSE AND IMPEDANCE CURVES W/ PLANE-WAVE TUBE. 1 mW

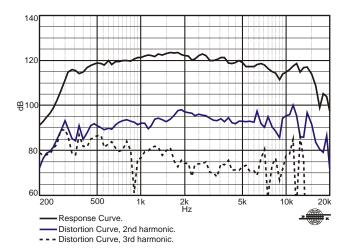


Frequency response and impedance curves measured with 50 mm terminated plane-wave tube, with sensitivity referenced to a 25 mm tube.

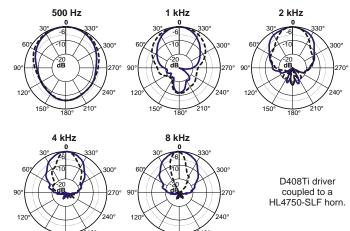
### HARMONIC DISTORTION CURVES W/ HL4750-SLF HORN, 1 W / 1 m.



#### HARMONIC DISTORTION CURVES W/ HL4750-SLF HORN, 10 W / 1 m.



#### **POLAR RESPONSE CURVES**



- Polar Response Curve, Horizontal.
- - Polar Response Curve, Vertical.

#### **HOW TO CHOOSE THE RIGHT AMPLIFIER**

The power amplifier must be able to supply twice the RMS driver power. This 3 dB headroom is necessary to handle the peaks that are common to musical programs. When the amplifier clips those peaks, high distortion arises and this may damage the transducer due to excessive heat. The use of compressors is a good practice to reduce music dynamics to safelevels.

### FINDING VOICE COIL TEMPERATURE

It is very important to avoid maximum voice coil temperature. Since moving coil resistance ( $R_{\scriptscriptstyle E}$ ) varies with temperature according to a well known law, we can calculate the temperature inside the voice coil by measuring the voice coil DC resistance:

$$T_B = T_A = \frac{R_B}{R_A} = 1 \quad T_A = 25 \quad \frac{1}{25}$$

 $T_A$ ,  $T_B$ = voice coil temperatures in °C.

 $R_{\scriptscriptstyle A}$  ,  $R_{\scriptscriptstyle B}$ = voice coil resistances attemperatures  $T_{\scriptscriptstyle A}$  and  $T_{\scriptscriptstyle B}$ , respectively.

= voice coil wire temperature coefficient at 25 °C.